

Ecohydrology

Daily Potential Evapotranspiration

Notation:	$PET=PE=E_o=ET_o$	[m d ⁻¹]
	T = temperature	[°K or °C]
	ρ_v = vapor density	[kg/m ³]
	ρ_v^o = saturation vapor density	[kg/m ³]
	e = vapor pressure = $4.26 \times 10^{-6} \rho_v T$	[mb]
		{T in °K}

I. Mass Balance

$$(1) \quad PET = \left(\frac{\rho_{vs}^o - \rho_{va}}{r_v} \right) \frac{1}{\rho_w} \quad [\text{m/s}]$$

ρ_{vs}^o	= saturated vapor density @ surface	[kg m ⁻³]
ρ_{va}	= vapor density of air	[kg m ⁻³]
ρ_w	= density of water	[10 ³ kg m ⁻³]
r_v	= resistance to vapor transfer, very sensitive to windspeed	[d/m]

$$(2) \quad r_v = \frac{\left(\ln \left(\frac{z-d+z_o}{z_o} \right) \right)^2}{uk^2} \sim \frac{\left(\ln \left(\frac{2}{z_o} \right) \right)^2}{uk^2} \quad \text{X } 86400 \text{ s/d}$$

u	= average windspeed	[m/s]
k	= von Karman Constant	[0.41]
z_o	= surface roughness (grass: $z_o = 0.5$ ish) $\sim 0.13h$	[m]
d	= zero plane displacement $\sim 0.77h$	[m]
h	= vegetation height	[m]

II. Energy Equations (Note energy is expressed in kJ)

Basic concept:

$$(3) \quad PET = \frac{Q_e}{\lambda_v \rho_w} \quad [\text{m d}^{-1}]$$

Q_e	= evaporative (latent) heat flux	[kJ m ⁻² d ⁻¹]
-------	----------------------------------	---------------------------------------

$$(4) \quad = \lambda_v \left(\frac{\rho_{vs}^o - \rho_{va}}{r_v} \right)$$

λ_v	= latent heat of vaporization	[2500 kJ kg ⁻¹]
-------------	-------------------------------	-----------------------------

Energy balance gives an estimate of Q_e :

$$(5) \quad Q_e = Q_{rn} - Q_h \quad [\text{kJ m}^{-2} \text{ d}^{-1}]$$

$$Q_{rn} = \text{net radiation energy flux} \quad [\text{kJ m}^{-2} \text{ d}^{-1}]$$

$$= \text{net solar radiation} + \text{atmospheric long wave radiation} - \text{terrestrial long wave}$$

$$Q_h = \text{Sensible heat flux} \quad [\text{kJ m}^{-2} \text{ d}^{-1}]$$

$$(6) \quad = C \left(\frac{T_s - T_a}{r_h} \right)$$

$$T_s = \text{temperature of the surface} \quad [^{\circ}\text{C}]$$

$$T_a = \text{air temperature} \quad [^{\circ}\text{C}]$$

$$r_h = \text{resistance to heat transfer} \approx r_v \quad [\text{d/m}]$$

$$C = \text{heat capacity of air} \quad [1.2 \text{ kJ m}^{-3} \text{ }^{\circ}\text{C}^{-1}]$$

Penman (1948, *Proc. Royal Soc.* A194:220) **Equation** simplifies the energy balance by removing all “surface” terms:

$$(7a) \quad Q_e = \frac{C \left(\rho_{va}^o - \rho_{va} \right) + \Delta Q_{rn}}{\gamma + \Delta} \quad [\text{kJ m}^{-2} \text{ d}^{-1}]$$

$$(7b) \quad Q_e = \frac{f(u) \left(\rho_{va}^o - \rho_{va} \right) + \Delta Q_{rn}}{\gamma + \Delta} \quad [\text{kJ m}^{-2} \text{ d}^{-1}]$$

$$\rho_{va}^o = \text{saturation vapor density at air temperature} \quad [\text{kg m}^{-3}]$$

$$\gamma \sim \text{psychrometric constant} \quad [4.95 \times 10^{-4} \text{ kg m}^{-3} \text{ }^{\circ}\text{C}^{-1}]$$

$$= \frac{C}{\lambda_v}$$

$$\Delta = \text{slope of the saturation curve on the psychrometric chart} \quad [\text{kg m}^{-3} \text{ }^{\circ}\text{C}^{-1}]$$

$$\approx 3.221 \times 10^{-4} \exp(0.08T^{0.8876}) \quad \text{for } 0 < T < 25^{\circ}\text{C} \quad [\text{kg m}^{-3} \text{ }^{\circ}\text{C}^{-1}]$$

$$\approx 3.405 \times 10^{-4} \exp(0.0642T) \quad \text{for } T < 0^{\circ}\text{C} \quad [\text{kg m}^{-3} \text{ }^{\circ}\text{C}^{-1}]$$

$$f(u) = \text{an empirical wind function that replaces } \frac{\lambda_v}{r_v} \quad [\text{kJ m kg}^{-1} \text{ d}^{-1}]$$

$$\sim 5.3(1 + u); u \text{ is the daily average windspeed [m/s] and measured at 2 m height.}$$

Note: Dunne and Leopold's (1978, *Water in Environmental Planning*) version of this equation (4-22) is for PET obtained by dividing equation (7) by $\lambda_v \rho_w$ (equation (4)) and using units of cal, g, days, and cm instead of kJ, kg, s, and m respectively. The Penmann approximation falls out in Dunne and Leopold's approach and is replaced by an empirical relationship, (4-22).

$$\text{Penman Approximation: } \rho_{vs} - \rho_{va} = \rho_{va}^o - \rho_{va} + \Delta(T_s - T_a)$$

Priestly-Taylor (1972, *Mon. Weather Rev.* 100:81-92) **equation** simplifies the Penman equation by assuming that the vapor deficit term and net radiation term are proportional.

$$(8) \quad \alpha' = \frac{\frac{C}{r_v} (\rho_{va}^o - \rho_{va})}{\Delta Q_{rn}} \quad [\text{kJ m}^{-2} \text{ d}^{-1}]$$

The resulting Priestly-Taylor equation uses a constant $\alpha = 1 + \alpha'$.

$$(9) \quad Q_e = \alpha \frac{\Delta Q_{rn}}{\gamma + \Delta} \quad [\text{kJ m}^{-2} \text{ d}^{-1}]$$

The common assumption is $\alpha = 1.26$.